

Research



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Fin sweep angle does not determine flapping propulsive performance

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The importance of the leading-edge sweep angle of propulsive surfaces used by unsteady swimming and flying animals has been an issue of debate for many years, spurring studies in biology, engineering, and robotics with mixed conclusions. In this work, we provide results from three-dimensional simulations on single-planform finite foils undergoing tail-like (pitch-heave) and flipper-like (twist-roll) kinematics for a range of sweep angles covering a substantial portion of animals while carefully controlling all other parameters. Our primary finding is the negligible 0.043 maximum correlation between the sweep angle and the propulsive force and power for both tail-like and flipper-like motions. This indicates that fish tails and mammal flukes with similar range and size can have a large range of potential sweep angles without significant negative propulsive impact. Although there is a slight benefit to *avoiding* large sweep angles, this is easily compensated by adjusting the fin's motion parameters such as flapping frequency, amplitude and maximum angle of attack to gain higher thrust and efficiency.

1. Introduction

A large fraction of swimming and flying animals use propulsive flapping to move, and there are significant potential applications for this biologically inspired form of propulsion in engineering and robotics. As such, significant research effort has been devoted towards understanding and optimizing both the kinematics and morphology of the propulsion surface itself, with a particular emphasis on explaining propulsive efficiency.

The leading edge sweep back angle is a key geometric feature observed in fish tails, mammal flukes, aquatic-animal flippers, and bird and insect wings. There have been extensive studies collecting sweep back angle data from a variety of animal propulsion surfaces. The data in figure 1 are collected from marine mammals [1], fish caudal fins [2], flyer wings [3–7] and aquatic-animal propulsive side-fins such as flippers [8–11], pectoral fins [12,13] and dorsal fins [14]. There is a strong correlation between fin aspect ratio, \mathcal{R} , and kinematics. Most tails in red colours (mammal flukes and caudal fins) are limited to the low to medium $\mathcal{R} < 7$ fins, where their median and average values are around $\mathcal{R} = 4$. The highest $\mathcal{R} \geq 8$ region is populated only by flippers and wings which perform rolling and twisting motions, such as penguins, turtle and most plesiosaurs. By contrast, the sweep angle Λ dependence is much less clear, with flipper and propulsive pectoral fins spanning a wide range of angles. While some individual studies indicate that increased sweep angles are correlated with animals with lower aspect ratio \mathcal{R} fins [15,16], there is extensive variation between animals within the groups and no strong trend is found when including all the groups using propulsive flapping. Additionally, there are hundreds of differences in the specific geometry and kinematics of each of these animals and just as many biological pressures other than propulsive efficiency at play, making it difficult to conclusively determine the influence of sweep angle from biological data directly.

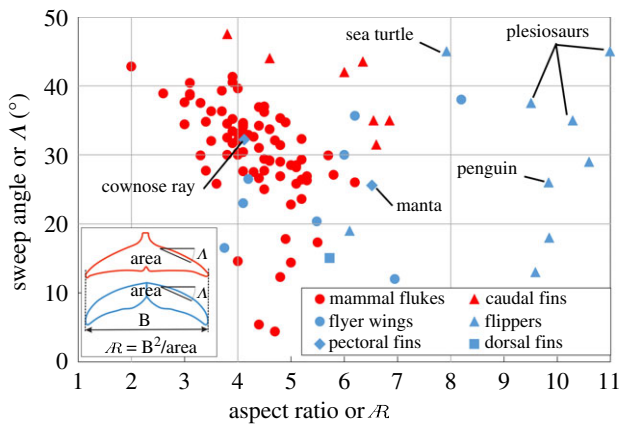


Figure 1. Collection of biological data for sweep angles Δ and aspect ratio for fish caudal fins and mammal flukes (in red) and wings, flippers, pectoral, and dorsal fins (in blue) showing the extremely wide scatter across this evolutionary parameter space for different successful animals. The current computational study takes place over sweep angles of 20, 30 and 40° and $AR = 2, 4, 8$ shown by grey lines to maximize the relevance to biological propulsive surfaces.

Focused engineering studies have also been applied to determine the impact of sweep angle on the performance of flapping propulsion surfaces. While these would hopefully clarify the issues at play, the findings are somewhat contradictory, especially between theoretical and experimental analysis. Most analytical studies using lifting-line theory indicate sweep is advantageous, increasing the thrust and propulsive efficiency [15–17]. While such methodologies are effective at determining lift characteristics on steady wings, they cannot model unsteady rotational three-dimensional flow, including the evolution of vortices that form at the fin's leading edge and tip which lead to the high forces observed in flapping foil propulsion [18,19].

While some experimental studies have measured a small flapping propulsive benefit to sweep, the effect is smaller than the analytic studies and other experiments have found no impact at all. A study on the spanwise flow caused by sweep angle found that it did not stabilize the leading-edge vortex (LEV) on an impulsively heaved foil [20], in contrast to the known stabilizing effect on a stationary wing. Another study reported affected forces and vortex strength on a 45°-sweptback flapping plate for large-scale LEVs produced by an impulsively heaved plate [21]. Insignificant force change is also seen in the experiment of manta robot with rolling flexible flippers [22]. Varying sweep angle from zero to 60° in rotating wings found no influence on the stability of the LEV [23]. For a purely pitching flat plate, the data of circulation time-histories show varying reduced frequencies can change the LEV circulation slightly more on the lower frequency cases [24]. This indicates that it is important to test a variety of kinematics relevant to the problem, as well as controlling for as many other parameters as possible, something which is very difficult to accomplish in physical experiments.

In this work, we carefully isolate the effect of varied sweep angles from all other geometric parameters to help address the conflicting and scattered results of previous biological, theoretical and experimental studies. Using three-dimensional unsteady numerical simulations, we add sweep to a simple base fin shape and test its flapping propulsive performance for two types of biologically inspired kinematics, i.e. tail-like and flipper-like motions (figure 2a).

We also test the combined impact of AR and sweep as well as other kinematic parameters such as motion types and amplitudes to determine the relative influence of sweep angle on propulsive flapping.

Specifically, we define our geometry to use a NACA0016 foil cross-section with chord length C , defined parallel to the inflow U_∞ , and thickness $D = 0.16C$. A rectangular planform is combined with a tapered elliptic tip with a length of $1C$. The sweep angle Δ , defined in figure 2, is varied from $\Delta = [20^\circ, 30^\circ, 40^\circ]$ to cover the most populated biological range, figure 1. As the sweep is adjusted, the tip-to-tip foil span B is adjusted to maintain the desired aspect ratio $AR = B^2/S_p$, where S_p is the planform area. As with sweep, we use a wide range of $AR = [2, 4, 8]$ to cover the AR range of propulsive surfaces found in nature. Our chosen ranges have covered a minimum of 95% for aspect ratio and 82% for sweep angle as well as the characteristic Re range from the population of animal data provided in figure 1. The chordwise Reynolds number $Re = \rho U_\infty C / \mu = 5300$, where ρ , μ are the fluid density and viscosity, is kept fixed to isolate influence of the geometry and kinematics. This Reynolds number is representative for a wide range of biological and robotic applications as the thrust and power coefficients of flapping foils at the same Strouhal number and similar offset drag are insensitive to the variation of chordwise Reynolds number between $Re \approx 5000$ and $Re \approx 500\,000$ [25,26]. A range of Reynolds numbers $Re = 1600$ – $150\,000$ is tested for a pitch-heave case (tail-like motion), at $AR = 4$, sweep angle 20° and 40° which shows only minor variation in propulsive coefficients of force and power (see electronic supplementary material).

The propulsive fin geometry is subjected to sinusoidal 'tail-like' and 'flipper-like' motions diagrammed in figure 2. The tail-like kinematics are inspired by biological data for fish caudal fins and mammal flukes and made up coupled heave and pitch motions (figure 2b). The flipper-like kinematics are inspired by aquatic animal pectoral flippers and bird/insect wings, and are made up twist and roll motions (figure 2c). Combining twist to roll acts as prescribed linear flexibility to rigid foil. The motion amplitude and frequency are quantified by Strouhal number $St = 2Af/U_\infty$ and reduced frequency $k^* = fl^*/U_\infty$, where f is the motion frequency, $2A$ is the total perpendicular amplitude envelop for the motion, and l^* is a length scale equal to the total inline extent L for tail-like motions and $B/2$ for flipper-like motions. The majority of the simulations use a fairly low-frequency $k^* = 0.3$ and high amplitude $2A = l^*$ condition to imitate the average mammal-fluke kinematics as reported in biological data [1], and the Strouhal number $St = 0.3$ is fixed in the middle of the optimal propulsive efficiency range [27]. A few special cases outside these conditions were also simulated: a flipper-like motion using higher $k^* = 0.6$ and $St = 0.6$ to imitate penguin and turtle swimming data with high roll and twist angles to maintain high propulsion and efficiency due to high AR . Also, a tail-like motion at lower amplitude $A = 0.13l^*$ and much higher frequency at $St = 0.46$ inspired by recent robotics studies at similar operating conditions [28,29].

2. Impact of sweep on wake structures and propulsive characteristics

A set of example simulation results for both tail-like and flipper-like motions are shown in figure 3, with the flow's vortex

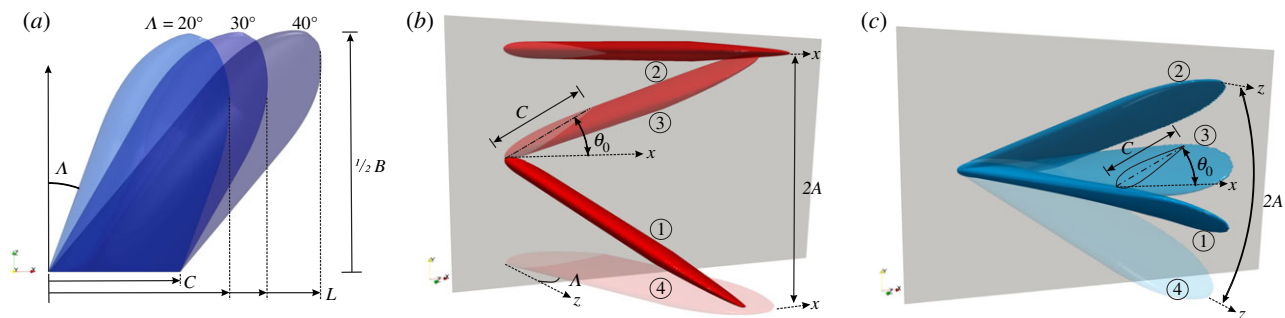


Figure 2. Diagram of the propulsive fin geometry and kinematics. (a) Foil planform with various sweep angles A for two different kinematics: (b) fishtail-like kinematics, i.e. pitch-heave combined with $AR = 4$ and (c) flipper-like kinematics, i.e. twist-roll combined with $AR = 8$. Phase steps per cycle are denoted from ① to ④.

structures visualized using the Q -criterion [29]. The complete unsteady flow field evolution can be viewed in the electronic supplementary material video. These wake visualizations show that small scale features such as the generation of small turbulent vortices depend on both the geometry and the kinematics. However, the large-scale underlying flow structures illustrated in the bottom row sketches are the same for a given set of kinematics; changing the sweep angle from 20° to 40° simply shifts and scales those structures. Specifically, for the tail-like motions in the left column, the LEV detaches from the top of the fin halfway along the inline length $l^* = L$ for tail-like motions. Similarly, while increasing the sweep angle pushes the LEV back for flipper-like motions, the separation for both cases occurs around 70% along the fin width $l^* = B/2$ for these cases. The period and wavelength of the trailing wake structures also scale with l^* because we have used l^* to define the reduced frequency k^* and the amplitude envelope $2A = l^*$. In other words, the sweep angle does not fundamentally change the resulting propulsive flow around the fins other than changing the characteristic length l^* .

We can quantify this invariance of the flow in terms of the integrated propulsive metrics: the coefficients of thrust C_T , lift C_L and power C_{Pow} and the propulsive efficiency η , defined as

$$C_T = \frac{F_x}{0.5\rho S_p U_\infty^2}, \quad C_L = \frac{F_y}{0.5\rho S_p U_\infty^2} \quad (2.1)$$

and

$$C_{Pow} = \frac{P}{0.5\rho S_p U_\infty^3}, \quad \eta = \frac{\overline{F_x} U_\infty}{\overline{P}} = \frac{\overline{C_T}}{\overline{C_{Pow}}} \quad (2.2)$$

where measured thrust force (F_x), lift force (F_y) and power (P) are calculated from the integration of pressure and viscous forces over the foil. S_p is the foil planform area and overline signifies cycle averaging.

A sample of the lift coefficient results are shown in figure 4 for both tail-like and flipper-like kinematics across the range of sweep angles. The qualitative and quantitative features of the lift force over the cycle are relatively unaffected by doubling the sweep angle. In particular, our simulation results do not indicate a significant time delay in the peak lift with sweep, meaning that sweep is not changing the stability of the propulsive LEV. This conclusion is supported by the similarity in the LEV appearance on $A20^\circ$ and $A40^\circ$ in figure 3.

The thrust coefficient and power also show a similar lack of influence of sweep on hydrodynamic performance. This

information is presented in the electronic supplementary material where we present the variation of mean thrust and lift coefficients (and their variance) as well as power coefficient (and its variance) and pitching moment for different AR and kinematics. These simulation results suggest that sweep causes slight variations in the breakdown of the main vortex structures but this is not observed to have significant impact on cycle-to-cycle force and moment variations.

Figure 5 summarizes the influence of the geometric and motion parameters on the propulsive characteristics across 39 simulation cases and clearly illustrates our primary finding that sweep angle is not responsible for the large potential variation in flapping propulsion. Here, the geometric parameters are the sweep angle and AR , whereas the kinematic parameters are the motion type (heave, roll, etc.) and flapping amplitude A/l^* . Different St and k^* are achieved using two flapping amplitudes: a high amplitude, low-frequency setting to mimic biological swimmer, and a low amplitude, high frequency setting to represent many robotic swimmers.

The cycle average thrust and power are shown in figure 5a,b. The motion type and amplitude produce large variations in these metrics (ranging from $\overline{C_T} \approx -0.4 \dots 0.8$ and $\overline{C_{Pow}} \approx 0 \dots 5.5$) whereas the propulsive outputs are found to be substantially invariant to alterations of sweep angle and AR . For positively propulsive cases ($\overline{C_T} > 0$), increasing sweep angle typically has an adverse effect on $\overline{C_T}$; the largest being a 0.07 decrease between $A20^\circ$ to $A40^\circ$ for the engineering-inspired (low amplitude and intermediate AR) pure pitch cases. Compensating this loss of thrust, these cases also see a reduction of 0.17 in the required $\overline{C_{Pow}}$ with increased sweep. By contrast, propulsive heave cases with engineering-inspired amplitude are seen to benefit from sweep angle with an increase of 0.03 in $\overline{C_T}$, but with the corresponding increase of 0.12 in $\overline{C_{Pow}}$. We also note that the propulsive tail-like motions produce relatively higher $\overline{C_T}$ than the flipper-like motions and that biological-inspired amplitude cases generally have lower $\overline{C_T}$ and $\overline{C_{Pow}}$ than engineering-inspired ones.

The propulsive efficiency is shown in figure 5c, which only includes configurations where $\overline{C_T}, \overline{C_P} \geq 0.05$ to avoid meaningless negative propulsive efficiencies and division by near-zero power (feathered conditions). As with the thrust and power, the impact of sweep angle on efficiency is found to be smaller than the motion parameters. The largest effects are a 5.6% efficiency decrease observed when increasing from $A20^\circ$ to $A40^\circ$ in the twist + roll (flipper-like)

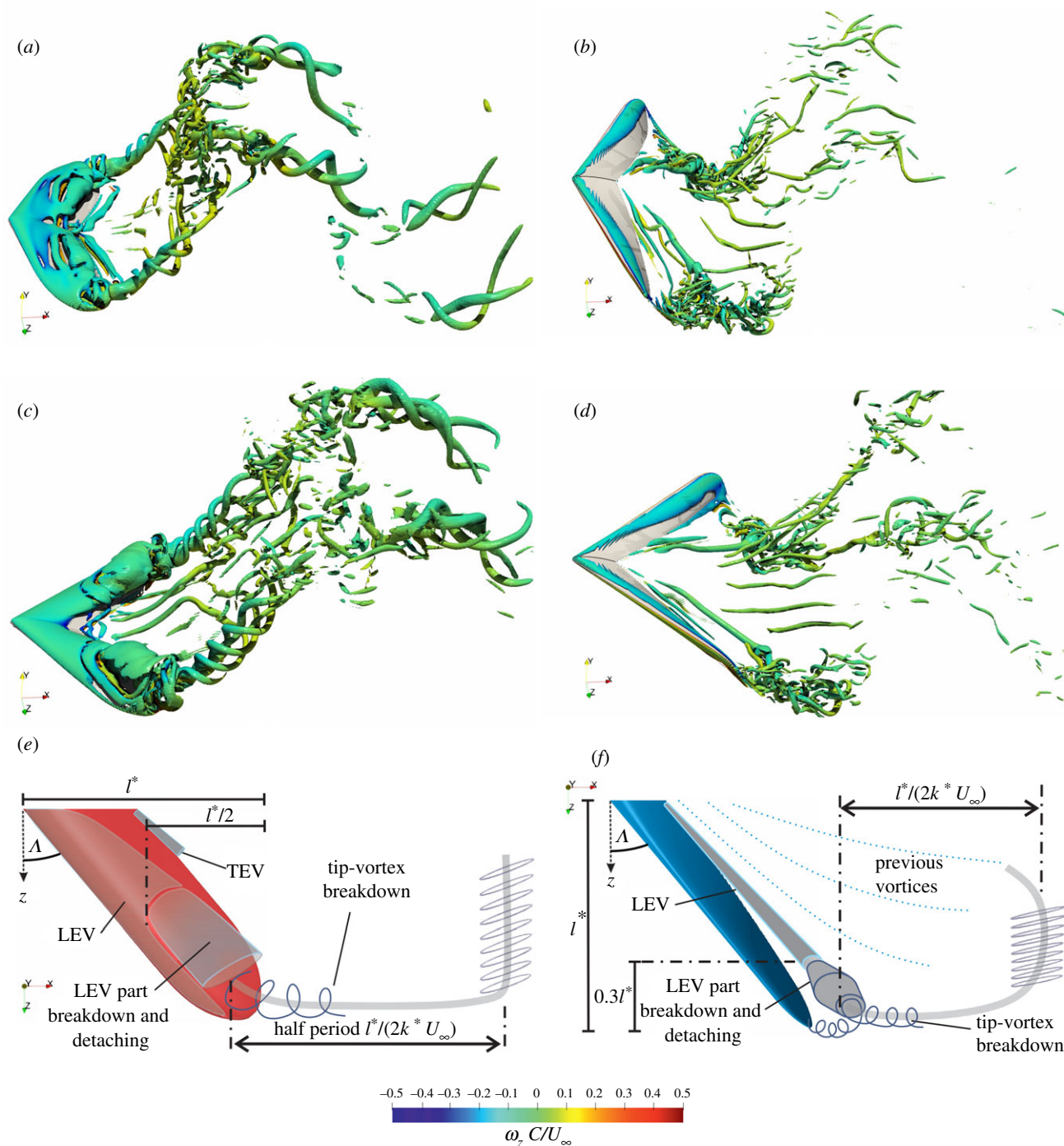


Figure 3. Flow structures generated by tail-like propulsive swimming at position ④ shown in figure 2b and flipper-like propulsive swimming at position ① shown in figure 2c. Tail-like motions are depicted in pitch-heave for (a) $\Lambda 20$, (c) $\Lambda 40$ for $\mathcal{R} = 4$, and flipper-like motions as in twist-roll for (b) $\Lambda 20$, (d) $\Lambda 40$ for $\mathcal{R} = 8$. Instantaneous vortex structures are visualized using iso-surfaces with 1% of Q_{\max} coloured by the spanwise vorticity $\omega_z C/U_\infty$. Illustration of vortex-shedding process every half period ($l^*/(2k * U_\infty)$) of cycle for (e) tail-like motion and (f) flipper-like motion.

case for $A/l^* = 0.5$ and a 3.4% efficiency reduction for the pitch (tail-like) cases for $A/l^* = 0.13$. By contrast, we see that kinematics made up of a combination of degrees of freedom (twist + roll, heave + pitch) are much more beneficial than single degree-of-freedom motions (pure pitch, heave or roll). The efficiencies above 25% belong to the cases with combined motions and higher amplitude (biological-inspired) conditions, with flipper-like motion giving the highest efficiency. This is caused by their lower $\overline{C_{\text{Pow}}}$ compared to engineering-inspired configurations. In addition, the penguin-like flipper case has a high $\approx 40\%$ efficiency which is achievable because the long span and large twist amplitude combine to achieve a similar maximum angle of attack along the span [30]. All types of

motion with lower amplitude (engineering-inspired) give efficiencies between 4 and 20% with pure heave giving lower efficiencies because of higher $\overline{C_{\text{Pow}}}$.

Overall, it is clear that kinematic parameters are more influential than the planform geometry for propulsive optimization. This can be summarized quantitatively using the correlations between the different input parameters and the propulsive outputs (figure 5d). The Pearson's correlation between the sweep angle and the propulsive statistics ranges from -0.043 to 0.001 , whereas all the amplitude and motion parameters are strongly correlated with all the force and power coefficients, with levels of 0.50 to 0.71 . The \mathcal{R} of the propulsive surface is also found to be secondary compared to the

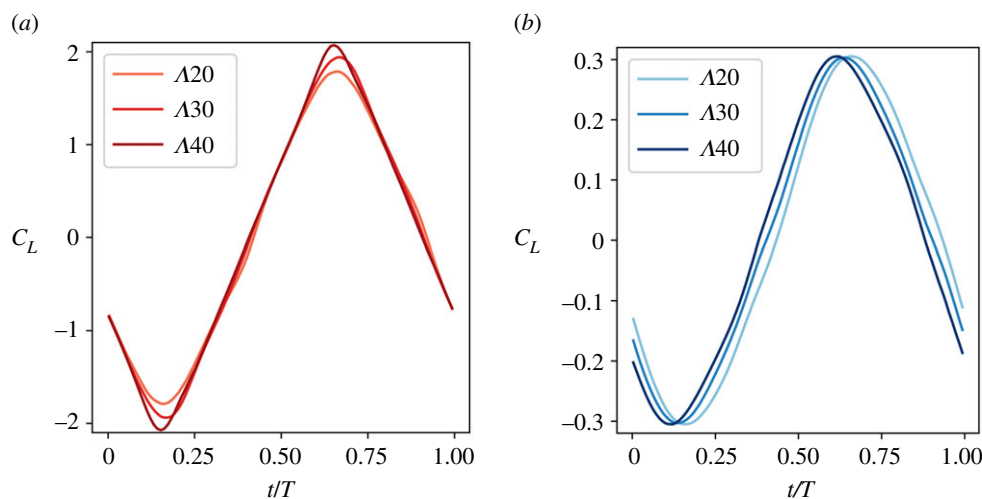


Figure 4. Lift coefficient of (a) tail-like and (b) flipper-like motion for $R = 4$, $St = 0.3$ and $k^* = 0.3$ in one cycle period (T). Both graphs show no LEV detachment delay as Λ increases.

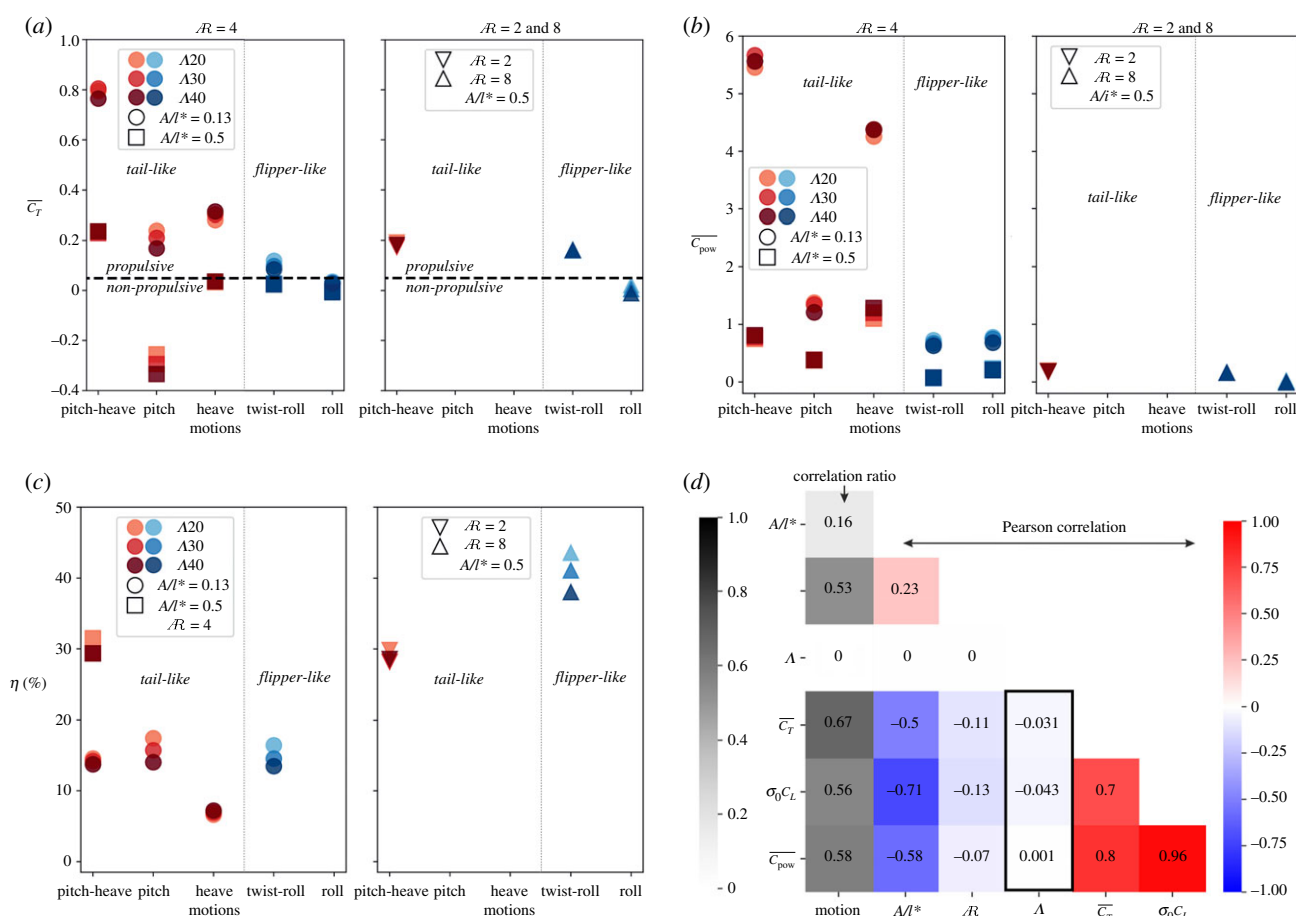


Figure 5. Results of 39 simulations are presented in different sweep angles Λ , aspect ratios R , motions, and A/l^* for (a) mean thrust coefficients \bar{C}_T , (b) mean power coefficients \bar{C}_{pow} and (c) propulsive efficiencies η for the thrust producing cases ($\bar{C}_T, \bar{C}_{pow} \geq 0.05$). Correlations among the various input and output parameters for \bar{C}_T , η , amplitude of the lift coefficient measured by the standard deviation $\sigma_0 C_L$, and \bar{C}_{pow} are presented in (d) a heat-map graph of correlation coefficients using Pearson and correlation ratio with a box highlighting Λ correlation. All graphs show that sweep angles have an insignificant impact on the output in spite of the large input variation evidenced by the correlation values in the boxes of (d). See an interactive graph in the electronic supplementary material for other input variations.

kinematics, with the largest absolute correlation of -0.13 between R and the standard deviation of the lift coefficient.

3. Conclusion

In conclusion, we have studied the influence of fin sweep angle and R on flapping foil propulsive performance using

a set of high resolution three-dimensional viscous flow simulations. This enables us to more tightly control all other geometric and kinematic parameters than would be possible in biological or experimental studies, producing an extensive and focused dataset of flow fields, integrated forces, and propulsive efficiencies. We have seen that sweep angle does not provide a significant advantage or disadvantage for tail-like

propulsive foils. This can explain why biological data for sweep angle of fish caudal fins and mammal flukes have a large observed range and are not strongly correlated with kinematics or fin aspect ratio. From a biological perspective, this signifies that the so-called fastest fishes from Scombridae family or mammals from Delphinidae family in figure 1 can have either high or low sweep angle given any \mathcal{AR} range without losing thrust and affecting their propulsive efficiency. Similarly, increased sweep angle does not give an advantage to flipper-like motions, instead tending to lose efficiency due to increased power requirements and loss of thrust. However, this loss is small, typically less than 10%, and can be compensated by increasing tip frequency, Strouhal number, and twist angle to recover the lost thrust force. The sweep angle also does not affect the lift coefficient, which is beneficial as flippers are also used as a lift regulator in animal swimming [31].

This study finds no benefit to sweep for steady-speed swimming, but this does not preclude other more subtle potential fluid dynamic advantages. For example, in very high-velocity motions more similar to animal manoeuvring than steady swimming [32], experiments have observed a modulated C_L peak for 145° compared to 10° [21]. In addition, previous simulations have shown that fin-to-fin interactions may have an important effect on increasing propulsive efficiency [33]. As such, it is still possible that sweptback angle may impart an advantage, despite not making a significant contribution to steady swimming efficiency. We do not address dynamic flexibility in this work, but we prove that the prescribed flexibility (twist) impacts greatly on the propulsive efficiency because it decreases side force $\sigma_0 C_L$ and power coefficient $\overline{C}_{\text{Pow}}$. However, the sweep angle is still invariant to the twist, explaining why manta and cownose-ray flexible pectoral fins are found in the middle of sweep angle and \mathcal{AR} ranges in figure 1 similar to most members of Scombridae and Delphinidae. This finding should help focus research in these more fruitful directions, and simplify the design of potential biologically inspired vehicles and robots.

4. Methods

The prescribed forms of the heaving $\mathcal{H}(t)$ and pitching $\theta(t)$ functions are given by

$$\mathcal{H}(t) = A \sin(2\pi ft) \quad (4.1)$$

$$\theta(t) = \theta_0 \sin(2\pi ft + \psi) \quad (4.2)$$

and
$$\theta_0 = \sin^{-1}(A/l^*), \quad (4.3)$$

where θ_0 is the trailing-edge tip rotation amplitude, and the phase difference $\psi = 90^\circ$ is set based on the maximum performance for two-dimensional motions [34]. The twist is defined

equivalently to pitch, with the amplitude increasing with distance from the root section. The pivot point of pitch and twist is at the leading edge of the root section. The roll motion is simply rotation about the inline axis, and the amplitude is set to achieve the same amplitude A at l^* similarly to maximum twist as described in [30].

The correlation data in figure 5d use the Pearson coefficient of correlation between two continuous sets of data, and the correlation ratio between a category set and a continuous dataset, defined as

$$\sqrt{\frac{\sum_x n_x (\bar{y}_x - \bar{y})^2}{\sum_{x,i} (y_{xi} - \bar{y})^2}}, \quad (4.4)$$

where

$$\bar{y}_x = \frac{\sum_i y_{xi}}{n_x} \quad \text{and} \quad \bar{y} = \frac{\sum_x n_x \bar{y}_x}{\sum_x n_x}, \quad (4.5)$$

x is the category in each observation y_{xi} , i is the index, n_x is the number of observations in category x and \bar{y}_x is the mean of category x .

The flow simulation package used for this research is the boundary data immersion method (BDIM) [35]. BDIM uses a robust and efficient Cartesian grid with an implicit LES (iLES) solver. BDIM uses analytic meta-equations for an immersed body in multi-phase flow with a smoothed interface domain using an integral kernel. BDIM has been validated, proved suitable for accurate force predictions on moving bodies such as flapping foils [36].

Symmetric conditions are enforced on both spanwise boundaries for the finite foil simulation. The domains extend from the pivot point to 4C at the front, 11C at the rear, 5.5C at the top and bottom. Meanwhile, the tip distance to the maximum spanwise domain is 3.2C. The grid convergence study provided in [19] using an infinite foil with a span length of 6C in $Re = 5300$ as a comparison of time-averaged thrust coefficient for different resolutions. The force coefficient converges to within 7% of the finer simulations (for two- and three-dimensional simulations) using a resolution of $C/\Delta x = 128$. As a balance between the grid resolution and the number of simulations, this resolution is deemed sufficient to capture the dynamics of the flow.

Data accessibility. Data published in this article are available from the University of Southampton repository at <https://doi.org/10.5258/SOTON/D1811> [37].

Competing interests. We declare we have no competing interests.

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References

1. Fish FE, Rohr JJ. 1999 Review of dolphin hydrodynamics and swimming performance. Technical report, SSC San Diego.
2. Magnuson JJ. 1978 Locomotion by scombrid fishes: hydromechanics, morphology, and behavior. In *Locomotion* (eds WS Hoar, DJ Randall), vol. 7, pp. 239–313. New York, NY: Academic Press.
3. Hubel TY, Hristov NI, Swartz SM, Breuer KS. 2016 Wake structure and kinematics in two insectivorous bats. *Phil. Trans. R. Soc. B* **371**, 20150385. (doi:10.1098/rstb.2015.0385)
4. Von Busse R, Hedenstrom A, Winter Y, Johansson LC. 2012 Kinematics and wing shape across flight speed in the bat, *leptonycteris yerbabuenae*. *Biol. Open* **1**, 1226–1238. (doi:10.1242/bio.20122964)
5. Klaassen van Oorschot B, Mistick EA, Tobalske BW. 2016 Aerodynamic consequences of wing morphing during emulated take-off and gliding in birds. *J. Exp. Biol.* **219**(Pt 19), 3146–3154. (doi:10.1242/jeb.136721)
6. Willmott AP, Ellington CP. 1997 The mechanics of flight in the hawkmoth *manduca sexta*. II. Aerodynamic consequences of kinematic and morphological variation. *J. Exp. Biol.* **200**(Pt 21), 2723–2745. (doi:10.1242/jeb.200.21.2723)

7. Pennycuik CJ. 1968 A wind-tunnel study of gliding flight in the pigeon *Columba livia*. *J. Exp. Biol.* **49**, 509–526. (doi:10.1242/jeb.49.3.509)
8. Fish FE, Battle JM. 1995 Hydrodynamic design of the humpback whale flipper. *J. Morphol.* **225**, 51–60. (doi:10.1002/jmor.1052250105)
9. Carpenter K, Sanders F, Reed B, Reed J, Larson P. 2010 Plesiosaur swimming as interpreted from skeletal analysis and experimental results. *Trans. Kansas Acad. Sci.* **113**, 1–34. (doi:10.2307/40588253)
10. Rivera AR, Rivera G, Blob RW. 2013 Forelimb kinematics during swimming in the pig-nosed turtle, *Carettochelys insculpta*, compared with other turtle taxa: rowing versus flapping, convergence versus intermediacy. *J. Exp. Biol.* **216**, 668–680. (doi:10.1242/jeb.079715)
11. Sato K, Shiomi K, Watanabe Y, Watanuki Y, Takahashi A, Ponganis PJ. 2010 Scaling of swim speed and stroke frequency in geometrically similar penguins: they swim optimally to minimize cost of transport. *Proc. Biol. Sci. B* **277**, 707–714. (doi:10.1098/rspb.2009.1515)
12. Russo RS, Blemker SS, Fish FE, Bart-Smith H. 2015 Biomechanical model of batoid (skates and rays) pectoral fins predicts the influence of skeletal structure on fin kinematics: implications for bio-inspired design. *Bioinspir. Biomim.* **10**, 046002. (doi:10.1088/1748-3190/10/4/046002)
13. Rambahiniarison JM, Araujo G, Lamoste MJ, Labaja J, Snow S, Ponzio A. 2016 First records of the reef manta ray *Manta alfredi* in the Bohol Sea, Philippines, and its implication for conservation. *J. Asia-Pacific Biodivers.* **9**, 489–493. (doi:10.1016/j.japb.2016.07.002)
14. Gurdek Bas R, Serra W, Trinchin R, Leoni V, Rubio L, Sampognaro L, Nagy G, Cravino A, Acuña A. 2015 Confirmation of *Mola mola* (Tetraodontiformes: Molidae) and historical records of ocean sunfishes (*Mola* sp.) in the coastal area of Uruguay. *Marine Biodivers. Records* **8**, 1–5. (doi:10.1017/s1755267214001468)
15. Chopra MG, Kambe T. 2006 Hydromechanics of lunata-tail swimming propulsion. Part 2. *J. Fluid Mech.* **79**, 49–69. (doi:10.1017/s0022112077000032)
16. Liu P, Bose N. 1993 Propulsive performance of three naturally occurring oscillating propeller planforms. *Ocean Eng.* **20**, 57–75. (doi:10.1016/0029-8018(93)90046-k)
17. van Dam CP. 1987 Efficiency characteristics of crescent-shaped wings and caudal fins. *Nature* **325**, 435–437. (doi:10.1038/325435a0)
18. Liu TS, Wang SZ, Zhang X, He GW. 2015 Unsteady thin-airfoil theory revisited: application of a simple lift formula. *AIAA J.* **53**, 1492–1502. (doi:10.2514/1.J053439)
19. Zurman-Nasution AN, Ganapathisubramani B, Weymouth GD. 2020 Influence of three-dimensionality on propulsive flapping. *J. Fluid Mech.* **886**, A25. (doi:10.1017/jfm.2019.1078)
20. Beem HR, Rival DE, Triantafyllou MS. 2011 On the stabilization of leading-edge vortices with spanwise flow. *Exp. Fluids* **52**, 511–517. (doi:10.1007/s00348-011-1241-9)
21. Wong JG, Kriegseis J, Rival DE. 2013 An investigation into vortex growth and stabilization for two-dimensional plunging and flapping plates with varying sweep. *J. Fluids Struct.* **43**, 231–243. (doi:10.1016/j.jfluidstruct.2013.09.010)
22. Arastehfar S, Chew CM, Jalalian A, Gunawan G, Yeo KS. 2019 A relationship between sweep angle of flapping pectoral fins and thrust generation. *J. Mech. Rob.* **11**, 011014. (doi:10.1115/1.4041697)
23. Lentink D, Dickinson MH. 2009 Rotational accelerations stabilize leading edge vortices on revolving fly wings. *J. Exp. Biol.* **212**(Pt 16), 2705–19. (doi:10.1242/jeb.022269)
24. Onoue K, Breuer KS. 2017 A scaling for vortex formation on swept and unswept pitching wings. *J. Fluid Mech.* **832**, 697–720. (doi:10.1017/jfm.2017.710)
25. Senturk U, Smits AJ. 2019 Reynolds number scaling of the propulsive performance of a pitching airfoil. *AIAA J.* **57**, 2663–2669. (doi:10.2514/1.1058371)
26. Schlichting H, Kestin J. 1979 *Boundary-layer theory*, 7th edn. New York, NY: McGraw-Hill.
27. Triantafyllou MS, Triantafyllou GS, Gopalkrishnan R. 1991 Wake mechanics for thrust generation in oscillating foils. *Phys. Fluids A* **3**, 2835–2837. (doi:10.1063/1.858173)
28. Zhu J, White C, Wainwright DK, Di Santo V, Lauder GV, Bart-Smith H. 2019 Tuna robotics: a high-frequency experimental platform exploring the performance space of swimming fishes. *Sci. Rob.* **4**, eaax4615. (doi:10.1126/scirobotics.aax4615)
29. King JT, Kumar R, Green MA. 2018 Experimental observations of the three-dimensional wake structures and dynamics generated by a rigid, bioinspired pitching panel. *Phys. Rev. Fluids* **3**, 034701. (doi:10.1103/PhysRevFluids.3.034701)
30. Zurman-Nasution AN, Ganapathisubramani B, Weymouth GD. 2021 Effects of aspect ratio on rolling and twisting foils. *Phys. Rev. Fluids* **6**, 013101. (doi:10.1103/PhysRevFluids.6.013101)
31. Cooper LN, Sedano N, Johansson S, May B, Brown JD, Holliday CM, Kot BW, Fish FE. 2008 Hydrodynamic performance of the minke whale (*Balaenoptera acutorostrata*) flipper. *J. Exp. Biol.* **211**(Pt 12), 1859–1867. (doi:10.1242/jeb.014134)
32. Read DA, Hover FS, Triantafyllou MS. 2003 Forces on oscillating foils for propulsion and maneuvering. *J. Fluids Struct.* **17**, 163–183. (doi:10.1016/S0889-9746(02)00115-9)
33. Han P, Lauder GV, Dong H. 2020 Hydrodynamics of median-fin interactions in fish-like locomotion: effects of fin shape and movement. *Phys. Fluids* **32**, 011902. (doi:10.1063/1.5129274)
34. Isogai K, Shinmoto Y, Watanabe Y. 1999 Effects of dynamic stall on propulsive efficiency and thrust of flapping airfoil. *AIAA J.* **37**, 1145–1151. (doi:10.2514/2.589)
35. Weymouth GD, Yue DKP. 2011 Boundary data immersion method for Cartesian-grid simulations of fluid-body interaction problems. *J. Comput. Phys.* **230**, 6233–6247. (doi:10.1016/j.jcp.2011.04.022)
36. Maertens P, Weymouth DD. 2015 Accurate Cartesian-grid simulations of near-body flows at intermediate Reynolds numbers. *Comput. Methods Appl. Mech. Eng.* **283**, 106–129. (doi:10.1016/j.cma.2014.09.007)
37. Zurman-Nasution AN, Ganapathisubramani B, Weymouth GD. 2021 Dataset for Fin sweep angle does not determine flapping propulsive performance. University of Southampton. (doi:10.5258/SOTON/D1811) (<http://dx.doi.org/10.5258/SOTON/D1811>)